

Equation sheet for Sensor Technologies exam

1. Error, signal-to-noise ratio and dynamic range:

$$\text{absolute error} = (\text{measured value}) - (\text{true value})$$

$$\text{relative error} = \frac{(\text{measured value}) - (\text{true value})}{\text{true value}}$$

$$\text{SNR} = 10 \log_{10} \left(\frac{P_{\text{signal}}}{P_{\text{noise}}} \right) = 20 \log_{10} \left(\frac{M_{\text{signal}}}{M_{\text{noise}}} \right)$$

$$\text{DR} = 10 \log_{10} \left(\frac{P_{\text{max}}}{P_{\text{noise}}} \right) = 20 \log_{10} \left(\frac{M_{\text{max}}}{M_{\text{noise}}} \right)$$

2. Propagating variance of x through $y = f(x)$:

$$\sigma_y^2 = \left(\left. \frac{\partial f}{\partial x} \right|_{x_0} \right)^2 \sigma_x^2$$

3. Propagating multiple variances through a vector-valued function $\mathbf{y} = f(\mathbf{x}) = f(x_1, \dots)$:

$$\Sigma_y = J \Sigma_x J^T$$

where J is the Jacobian evaluated at the given \mathbf{x} values, Σ_y is the covariance of \mathbf{y} , and Σ_x is the covariance of \mathbf{x} . In the case that y is a scalar and all variables are uncorrelated,

$$\sigma_y = \sqrt{\left(\frac{\partial f}{\partial x_1} \right)^2 \sigma_{x_1}^2 + \left(\frac{\partial f}{\partial x_2} \right)^2 \sigma_{x_2}^2 + \dots}$$

4. Jacobians:

$$J = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} & \dots \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} & \dots \\ \vdots & \vdots & \ddots \end{bmatrix}_{\mathbf{x}=\mathbf{x}_0}$$

5. Covariance matrix for 2 variables x_1 and x_2 :

$$\Sigma = \begin{bmatrix} \sigma_{x_1}^2 & \rho \sigma_{x_1} \sigma_{x_2} \\ \rho \sigma_{x_1} \sigma_{x_2} & \sigma_{x_2}^2 \end{bmatrix},$$

where σ is the standard deviation and ρ is the correlation.

6. Kalman filter:

$$\text{Predicted state: } \hat{\mathbf{x}}_{k|k-1} = F_k \hat{\mathbf{x}}_{k-1} + B_k \mathbf{u}_k$$

$$\text{Predicted cov.: } P_{k|k-1} = F_k P_{k-1} F_k^T + Q_k$$

$$\text{Measurement res.: } \mathbf{y}_k = \mathbf{z}_k - H_k \hat{\mathbf{x}}_{k|k-1}$$

$$\text{Measurement res. cov.: } S_k = H_k P_{k|k-1} H_k^T + R_k$$

$$\text{Kalman gain: } K_k = P_{k|k-1} H_k^T S_k^{-1}$$

$$\text{Updated state: } \hat{\mathbf{x}}_k = \hat{\mathbf{x}}_{k|k-1} + K_k \mathbf{y}_k$$

$$\text{Updated covariance: } P_k = (I - K_k H_k) P_{k|k-1}$$

7. Extended Kalman filter:

$$\text{Predicted state: } \hat{\mathbf{x}}_{k|k-1} = f(\hat{\mathbf{x}}_{k-1}) + b(\mathbf{u}_k)$$

$$\text{Measurement res.: } \mathbf{y}_k = \mathbf{z}_k - h(\hat{\mathbf{x}}_{k|k-1})$$

Let F_k and H_k be the Jacobians of f and h respectively.

8. Piezoresistive sensors (strain gauges):

$$\sigma = \frac{F}{A}, \quad \epsilon = \frac{\Delta L}{L_0}, \quad \sigma = E \epsilon, \quad \frac{\Delta R}{R_0} = G \epsilon$$

where σ is stress (N/m²), F is force, A is area, ϵ is strain, L is length (m), E is Young's modulus, R is resistance and G is gauge factor.

9. Temperature coefficient of resistance:

$$\text{TCR} = \frac{\left(\frac{dR}{dT} \right)}{R}$$

10. Self-heating of RTDs:

$$\Delta T = \frac{P_D}{\delta}$$

where ΔT is the self-heating error, P_D is the power dissipated in the RTD and δ is the heat dissipation constant.

11. Resistance, capacitance and inductance:

$$R = \frac{\rho l}{A}$$

$$C = \frac{\epsilon A}{d}, \quad \epsilon = \epsilon_r \epsilon_0, \quad \epsilon_0 = 8.85 \text{ pF/m}$$

$$L = \frac{\mu N^2 A}{l}, \quad \mu = \mu_r \mu_0, \quad \mu_0 = 4\pi \times 10^{-7} \text{ H/m}$$

where ρ is resistivity, l is length, A is cross-sectional area, ϵ is permittivity, ϵ_r is relative permittivity, d is distance, μ is permeability, and N is the number of wire turns in a solenoid.

12. Maxwell capacitance matrix:

$$\mathbf{Q} = \mathbf{C}\mathbf{V}$$

where $\mathbf{Q} = (Q_1 \dots Q_N)^T$ is the charge on each conductor and $\mathbf{V} = (V_1 \dots V_N)^T$ is the voltage on each conductor.

13. Mutual capacitances can be calculated from the Maxwell capacitance matrix using

$$C_{m,ii} = C_{ii} - \sum_{\substack{k=1 \\ k \neq i}}^N C_{m,ik}$$

$$C_{m,ij} = -C_{ij}$$

14. Thermocouple voltage:

$$V = E(T_{sense}) - E(T_{ref})$$

where E is the thermocouple characteristic function.

15. Transimpedance amplifiers:

$$C_f = \sqrt{\frac{C_{in}}{\pi R_f f_T}}$$

$$f_{-3dB} \approx \sqrt{\frac{f_T}{2\pi R_f C_{in}}}$$

where C_f is the capacitance along the op-amp feedback path, C_{in} is the total capacitance at the op-amp input, R_f is the resistance along the op-amp feedback path, and f_T is the op-amp's gain-bandwidth product.

16. Piezoelectric sensors:

$$\text{Sensor equation: } \mathbf{D} = [d] \mathbf{T} + [\epsilon] \mathbf{E}$$

$$\text{Actuator equation: } \mathbf{S} = [d]^T \mathbf{E} + [s] \mathbf{T}$$

where \mathbf{D} is electric displacement, $[d]$ is the 3×6 piezoelectric charge coefficient matrix, \mathbf{T} is stress, \mathbf{E} is electric field, \mathbf{S} is strain and $[s]$ is elastic compliance.

17. Hall effect sensors:

$$\mathbf{F} = q\mathbf{v} \times \mathbf{B}, \quad V_H = G_H \frac{iB}{qN_c L}$$

where $q = \pm 1.602 \times 10^{-19}$ C is the charge of a hole or electron, \mathbf{v} is charge carrier velocity, \mathbf{B} is the magnetic field vector and B is the component of magnetic field perpendicular to both the current and electric field, $G_H \approx 0.7$ to 0.9 is the geometry factor, i is current, L is the thickness of the sensor (in the direction of \mathbf{B}), and N_c is the charge carrier density in the semiconductor.

18. Eddy current skin depth:

$$\delta = \sqrt{\frac{2\rho}{\omega\mu}}$$

where ρ is resistivity, $\omega = 2\pi f$ is natural frequency, and $\mu = \mu_r \mu_0$ is permeability.

19. Linear variable differential transformers (LVDTs) have a transfer function of the form

$$V_0 = S V_i x$$

where V_0 is the output voltage, S is sensitivity, V_i is input voltage, and x is the displacement.

20. First order RC filters:

$$f_{-3dB} = \frac{1}{2\pi RC}$$